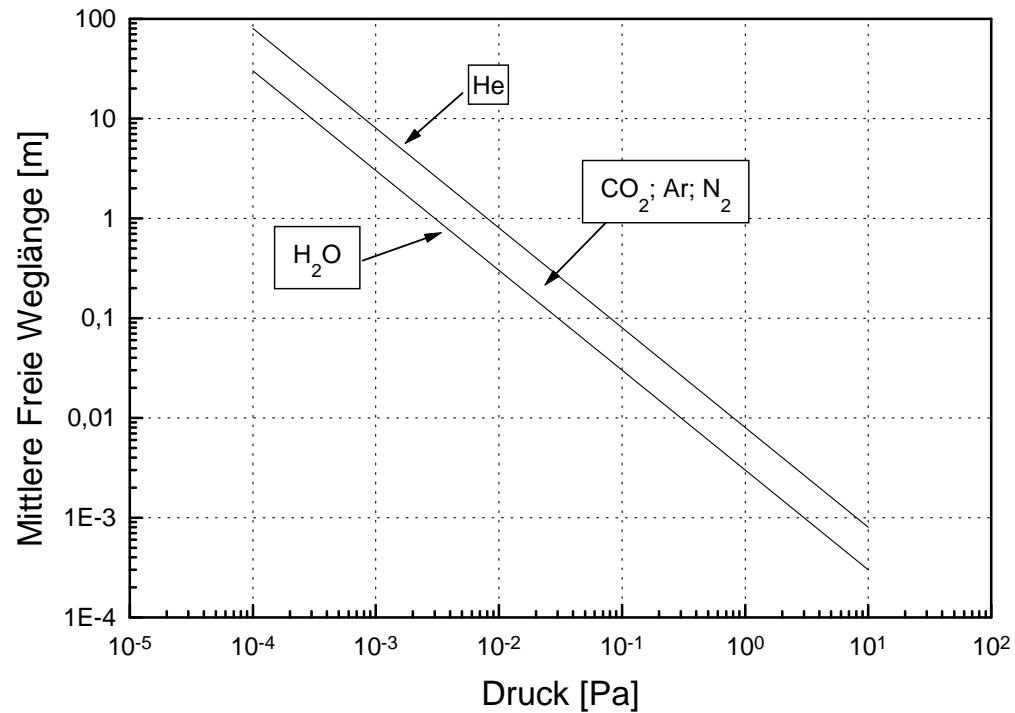


Repetition: Mean Free Path

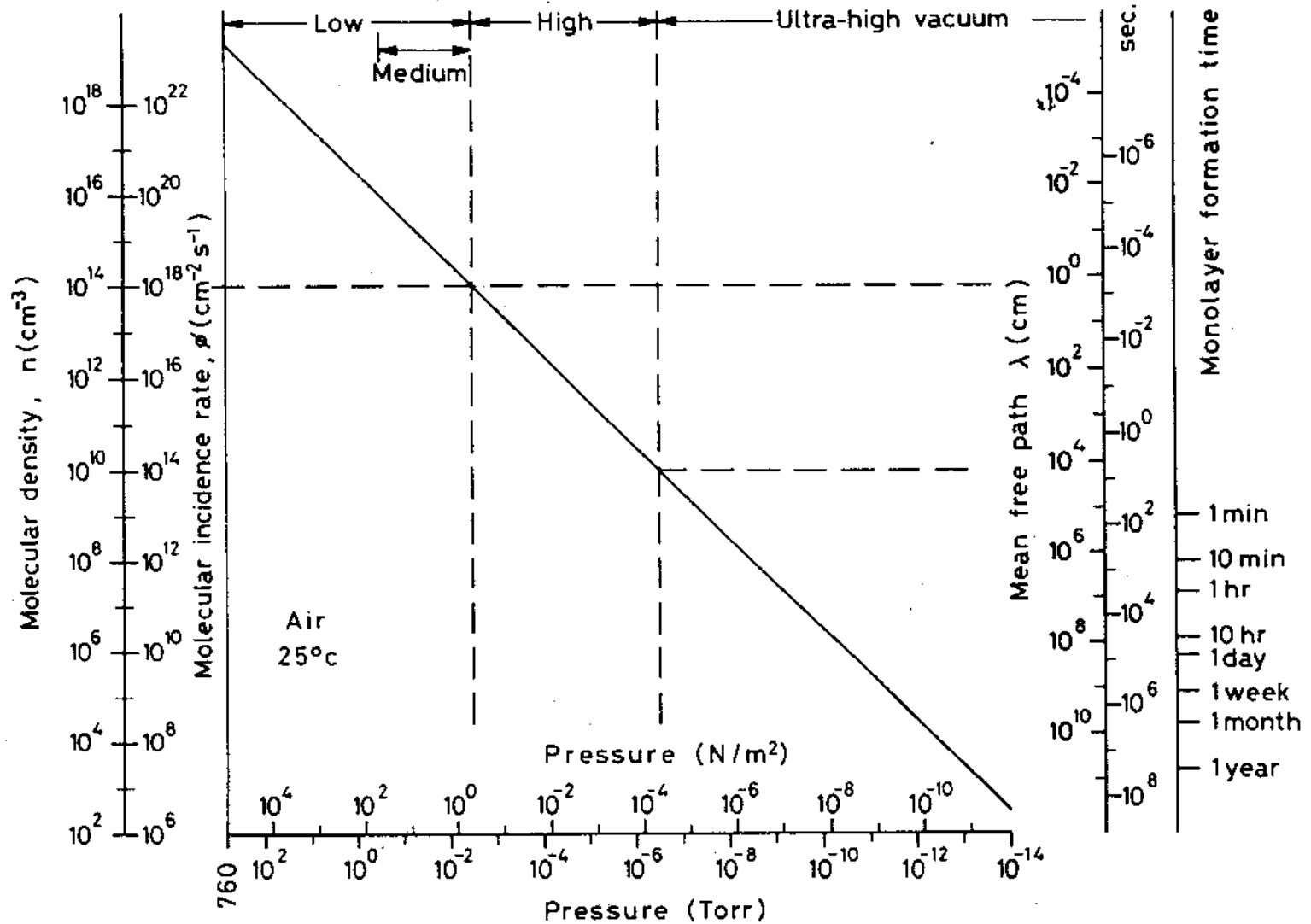
$$\lambda p = 5 \text{ mm Pa}$$

$$p = 1 \text{ Pa} \rightarrow \lambda = 5 \text{ mm}$$

$$p = 10^{-4} \text{ Pa} \rightarrow \lambda = 50 \text{ m}$$



Repetition: Areal Impingement Rate



Repetition: Design Criteria

- **Mean free path λ :**

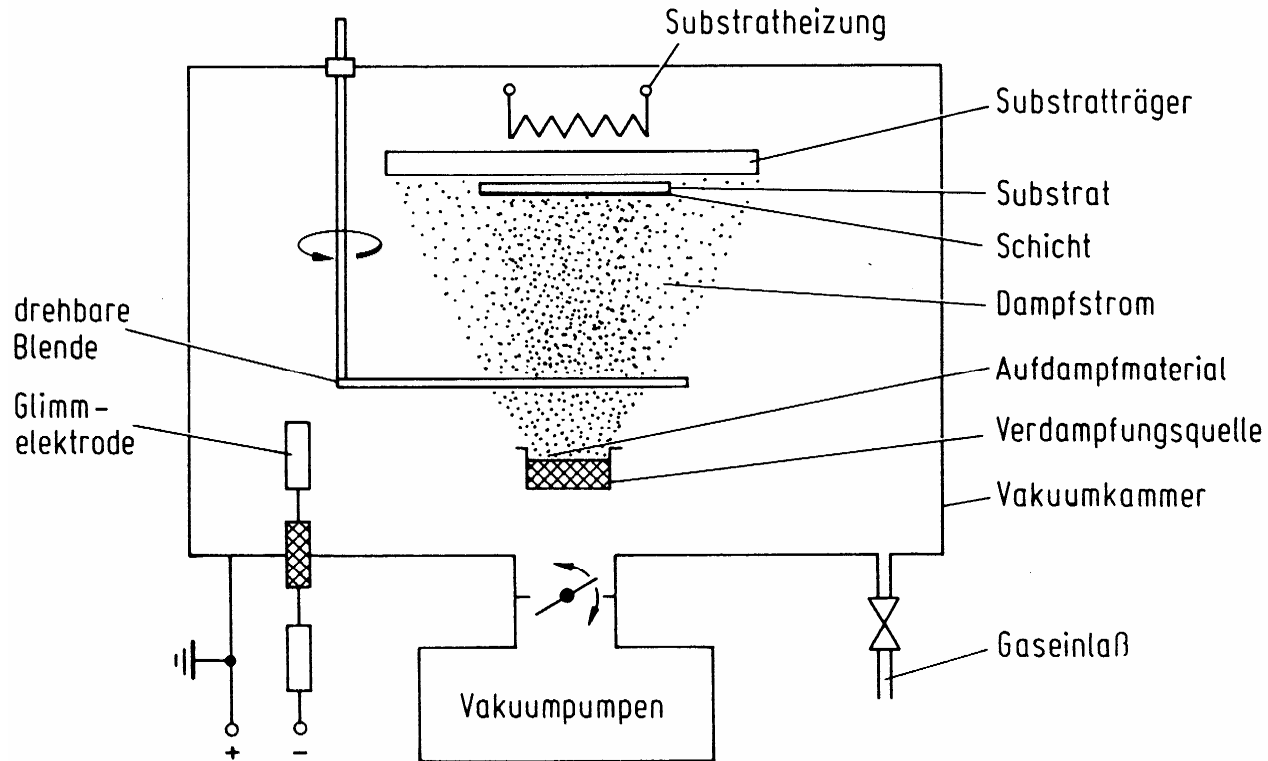
Influences gas dynamics. Even at rather high pressures (10^{-2} Pa) the mean free path reaches the dimensions of average deposition chambers .

- **Areal impingement rate Z:**

Crucial for coating purity. The pressure of the background gas has to be at least in the medium high vacuum to guarantee sufficient film purity.

Evaporation

Schematic:



Evaporation Rate: Temperature Dependence

$$Z = Z(p, T, m) = a_v \frac{p^* - p}{m} \sqrt{\frac{m}{2\pi k_B T}}$$

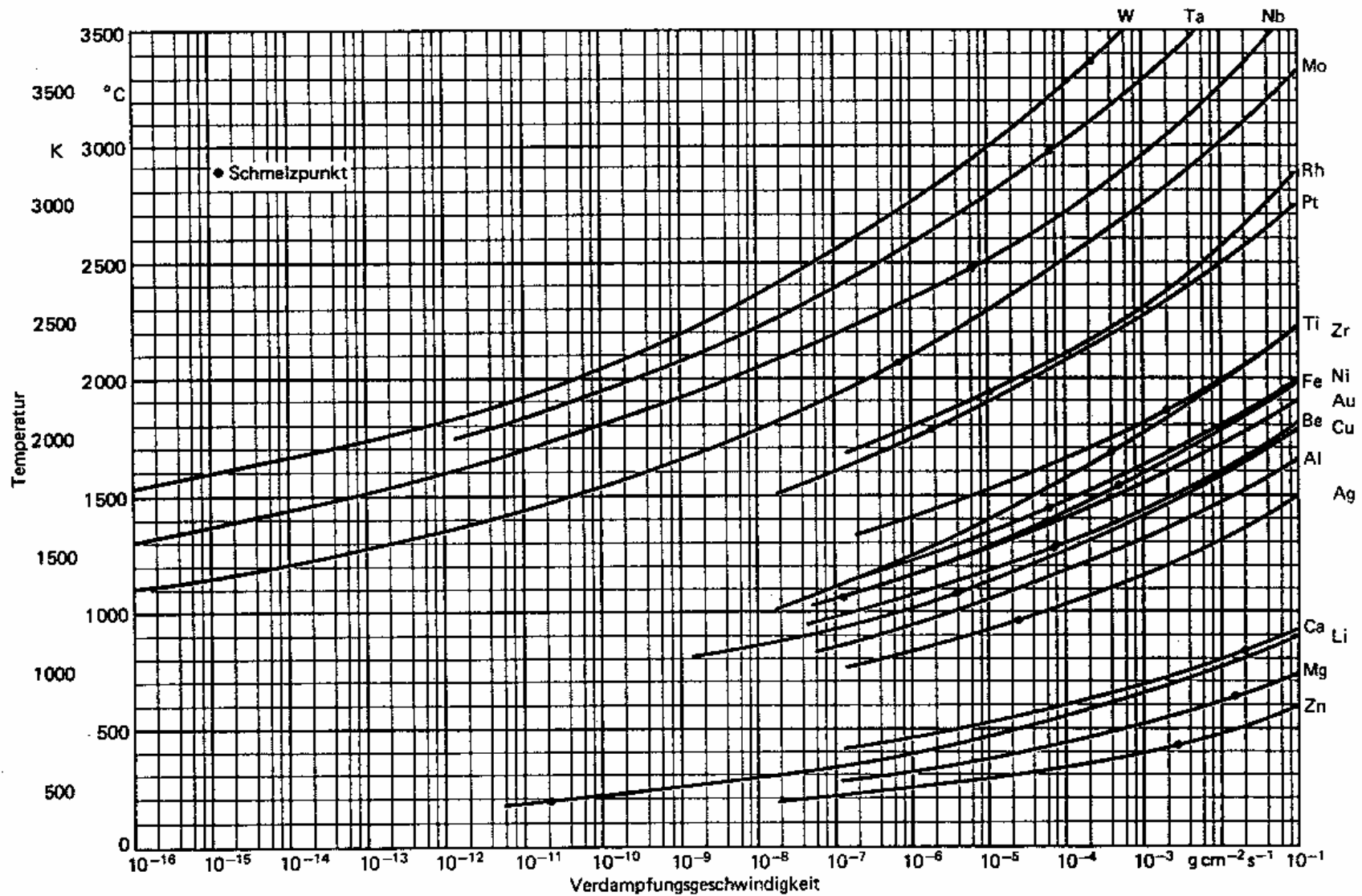
p^* = Temperature dependent vapor pressure of the source material
 a_v = Evaporation coefficient

$$p^* = p_0 \exp[-(E_V / (k_B T_Q))]$$

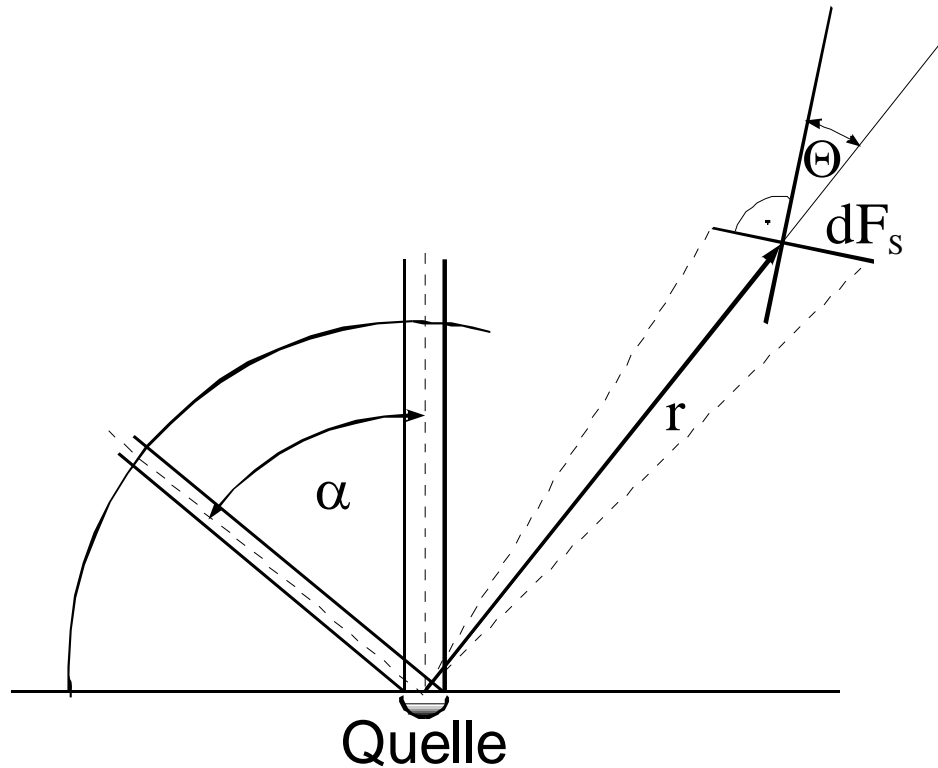
T_Q = Source temperature

p_0 = Reference vapor pressure, e. g. at room temperature (RT)

Evaporation Velocity Curves



Spatial Distribution of Vapor Streams



$$\Phi(\alpha) = \frac{dm}{d\Omega} = \frac{m_1}{\pi} \cdot \cos \alpha$$

Substrate tilt:

$$R(\alpha, \theta, r) = \Phi(\alpha) \cdot \cos \Theta \cdot \frac{1}{r^2}$$

Infinitesimal mass dm emitted into the solid angle:

$$dm = \frac{m_1}{\pi} \cdot \cos \alpha \cdot d\Omega$$

$$d\Omega = \frac{dA}{r^2} = \sin \alpha \cdot d\alpha \cdot d\varphi$$

Normalization:

$$\int_0^{2\pi} d\varphi \int_0^{\frac{\pi}{2}} \sin \alpha \cdot \cos \alpha \cdot d\alpha =$$

$$= 2 \cdot \pi \cdot \int_0^1 u \cdot du = 2 \cdot \pi \cdot \frac{1}{2} = \pi$$

$$\Rightarrow \int_{d\Omega} dm = m_1$$

Hertz-Knudsen Equation

$$R(\alpha, \theta, r) = \frac{m_1}{\pi} \cdot \cos \alpha \cdot \frac{\cos \Theta}{r^2}$$

Special geometries:

Plane substrate:

$$R(\alpha, \theta, r) = \frac{m_1}{a^2 \cdot \pi} \cdot \cos^4 \alpha$$

Half sphere:

$$R(\alpha, \theta, r) = \frac{m_1}{\pi \cdot a^2} \cdot \cos \alpha$$

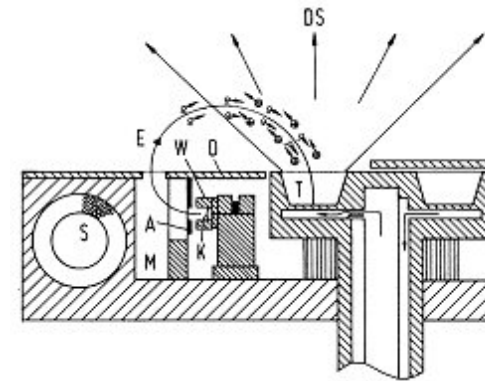
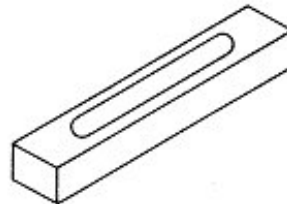
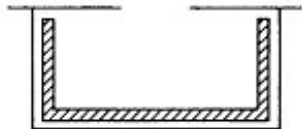
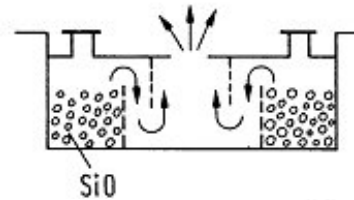
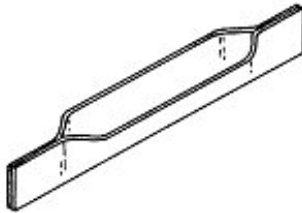
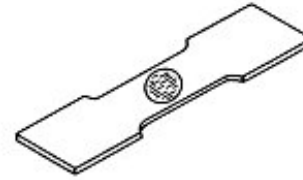
**Source in pole
(Knudsen-sphere):**

$$R(\alpha, \theta, r) = \frac{m_1}{\pi} \cdot \frac{1}{4 \cdot a^2} = \text{const}$$

a ... Distance or radius of the respective spheres

Evaporation Sources

Resistivity heated sources:



Electron gun

Vapor Pressure in Alloys I

Raoult's law:

Assumption: alloy A/B is ideal solution:

$$W_{AA} = W_{BB} = W_{AB}$$

Statement: vapor pressure of the materials
in solution is smaller than in the pure state:

$$p_A^* < p_A$$

* ... in solution

Vapor Pressure in Alloys II

Proof of Raoult's law:

$$p_A^* = \int \underbrace{m_A \cdot u_A}_{\text{momentum}} \cdot \underbrace{n_A \cdot u_A \cdot \Phi(u_A)}_{\text{differential collision rate}} \cdot du_A$$

$$p_A = \int n \cdot m_A \cdot u_A \cdot u_A \cdot \Phi(u_A) \cdot du_A$$

$$p_A^* = \frac{n_A}{n} \int n_A \cdot m_A \cdot u_A^2 \cdot \Phi(u_A) \cdot du_A$$

$$p_A^* = \frac{n_A}{n} \underbrace{\int n \cdot m_A \cdot u_A^2 \cdot \Phi(u_A) \cdot du_A}_{p_A}$$

$$p_A^* = \frac{n_A}{n} \cdot p_A$$

Raoult's law of vapor pressure reduction in solutions

Vapor Pressure in Alloys III

Raoult's law of vapor pressure reduction in **ideal** solutions:

$$p_A^* = \frac{n_A}{n} \cdot p_A$$

Raoult's law of vapor pressure reduction in **non-ideal** solutions:

$$p_A^* = f_A \cdot \frac{n_A}{n} \cdot p_A$$

f_A ... coefficient of activity

Evaporation of Alloys - Prerequisites

- **Prerequisite 1:**

Raoult's law of vapor pressure reduction in solutions is valid. The alloy is assumed to be an ideal solution.

- **Prerequisite 2:**

The solution is homogenous during the whole duration of the evaporation process. This means that the constituents are homogeneously distributed within the melt. There is no difference in the composition between surface and volume of the melt.

Evaporation of Alloys I

$$\frac{dN}{dA \cdot dt} = \frac{p}{\sqrt{2 \cdot \pi \cdot m \cdot k_B \cdot T}} = R_{\text{evap}} [\text{m}^{-2} \cdot \text{s}^{-1}]$$

$$\frac{dN}{dA} = dn \quad \text{Particles evaporate from the surface only}$$

$$\frac{dn_A}{dt} = \frac{p_A^*}{\sqrt{2 \cdot \pi \cdot m_A \cdot k_B \cdot T}} \quad p_A^* = \frac{n_A}{n} \cdot p_A$$

$$\frac{dn_B}{dt} = \frac{p_B^*}{\sqrt{2 \cdot \pi \cdot m_B \cdot k_B \cdot T}} \quad p_B^* = \frac{n_B}{n} \cdot p_B$$

Evaporation of Alloys II

Ratio of the changes of particle numbers in the melt

$$\frac{dn_A}{dn_B} = \frac{p_A}{p_B} \underbrace{\sqrt{\frac{m_B}{m_A}}}_{\kappa} \cdot \frac{n_A}{n_B} = \kappa \cdot \frac{n_A}{n_B}$$

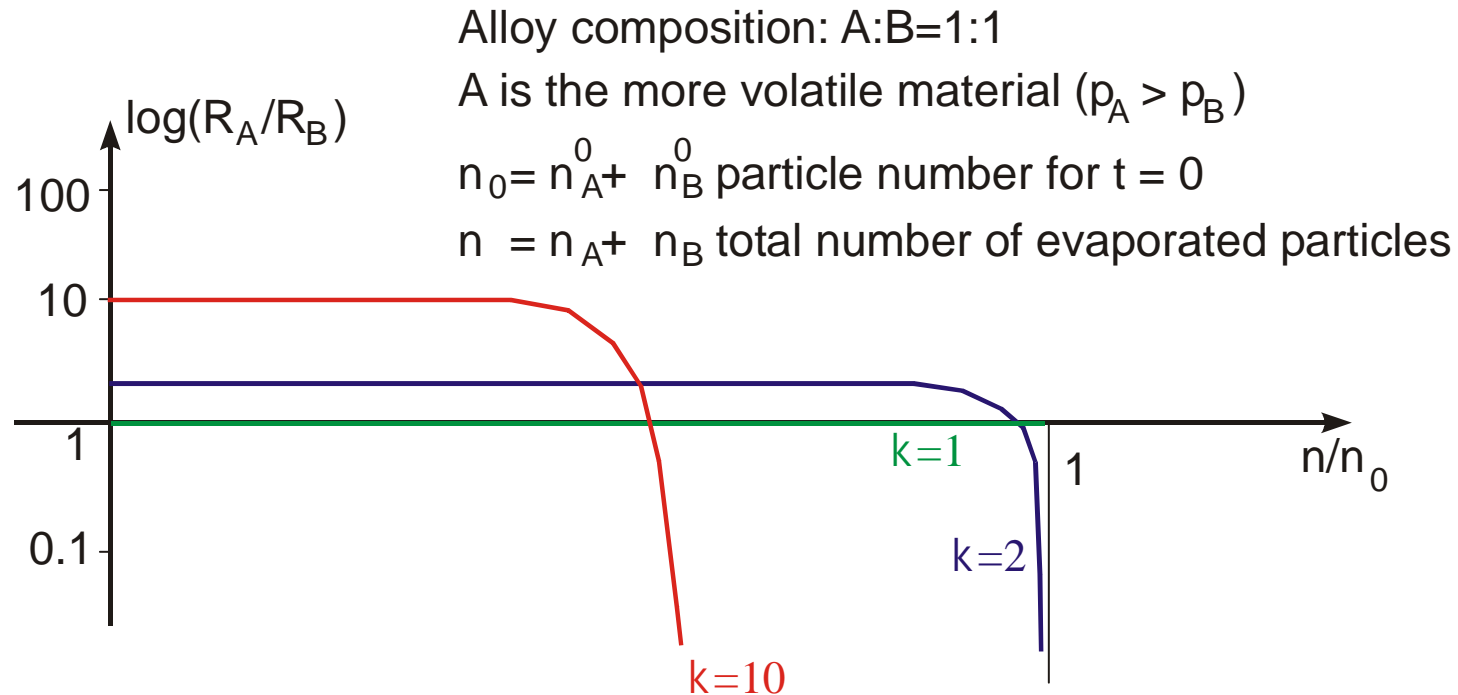
$n_A, n_B =$ Material content of material A, B

$p_A, p_B =$ Vapor pressure of A, B

$m_A, m_B =$ Mass of A, B

$\kappa =$ Evaporation coefficient

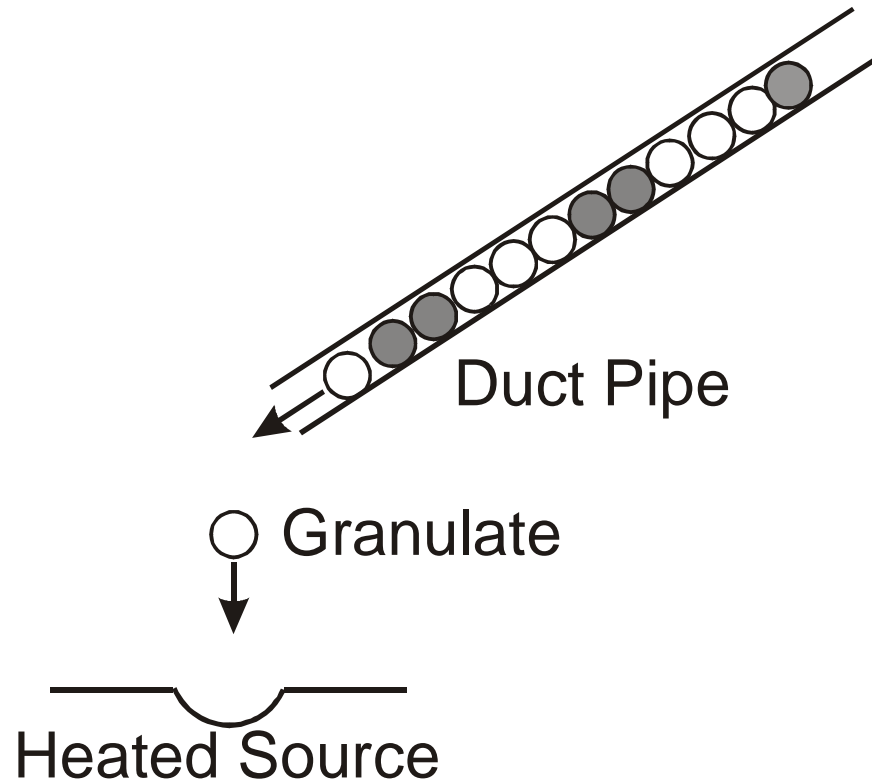
Evaporation of Alloys III



Evaporation of an alloy corresponds to a fractional distillation. The reason for this is the unhindered material transport within the source.

Special Evaporation Processes

Flash-evaporation



Multi-source-evaporation

Evaporation Materials

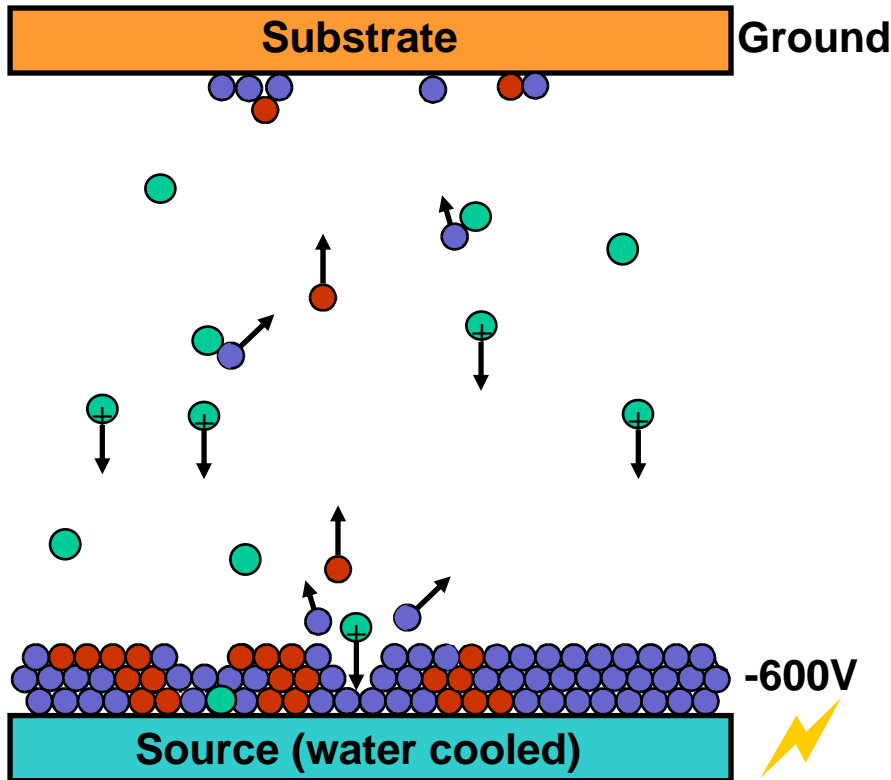
Powders
Granulates
Wires
Pellets
Shape parts



It is important, that the source material and the evaporation material do not chemically react with each other!

Sputtering

Elementary Processes:



Characteristics:

- **Solid source, i. e. arbitrary source geometry**
- **Low deposition temperature**
- **High deposition rates can be reached**
- **Wide parameter field**
- **Coating composition = source composition**
- **Good coating adhesion**
- **Interesting film properties**

Sputtering - Particle Ejection

Projectiles:

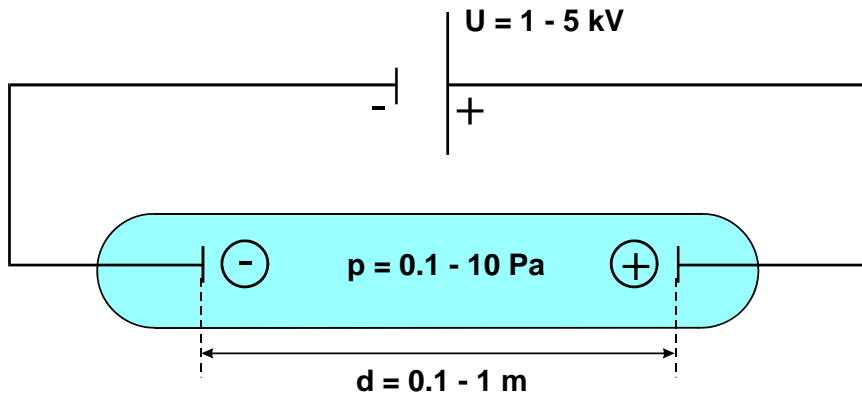
- Gas discharge
- Ion gun

Nature of ejected particles:

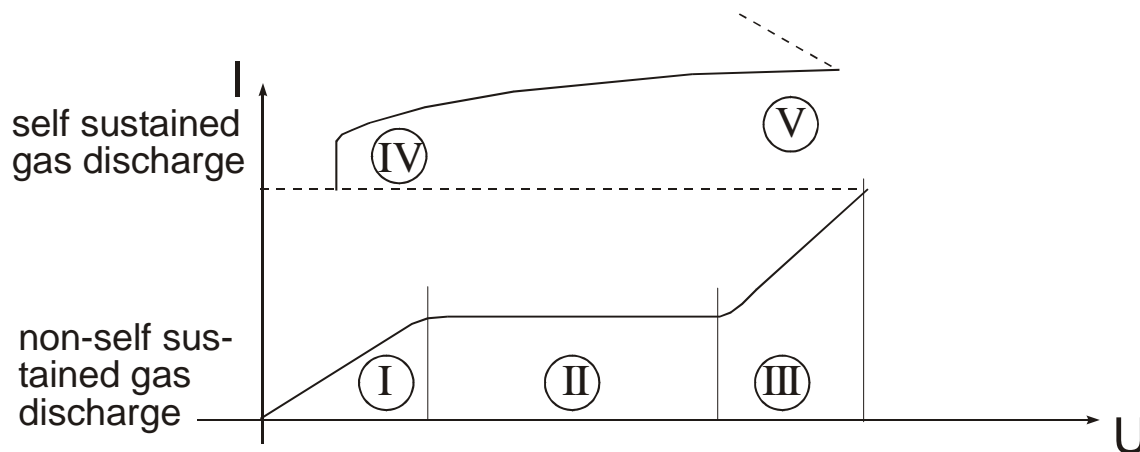
- Atoms
- Ions
- Cluster
- Molecules
- Secondary electrons

Gas Discharge - Basics

Experimental set-up:



I/V characteristic:



- I: Ohmic behavior
- II: Saturation region
- III: collisional ionization/
Townsend-discharge
- IV: normal glow
- V: anormal glow
secondary electron
emission

Gas Discharge (Diode Discharge) - Estimate

Basic mechanism of a gas discharge: **electrons** in a **diluted gas** ($p = 0.1 - 10 \text{ Pa}$) gain enough energy for **collisional ionization** of the gas atoms within their **mean free path λ** by applying a **voltage** in the **kV-region**.

Estimate:

$$p = 1 \text{ Pa}$$

$$E_{\text{ion}} = 10 \text{ eV} = W_{\text{el}}$$

$$\text{Electrode distance } d = 1 \text{ m}$$

Wanted:

Potential U

$$\lambda_{1\text{Pa}} = 5 \text{ mm}$$

$$W_{\text{el}} = E \cdot e \cdot \lambda = \frac{U}{d} \cdot e \cdot \lambda$$

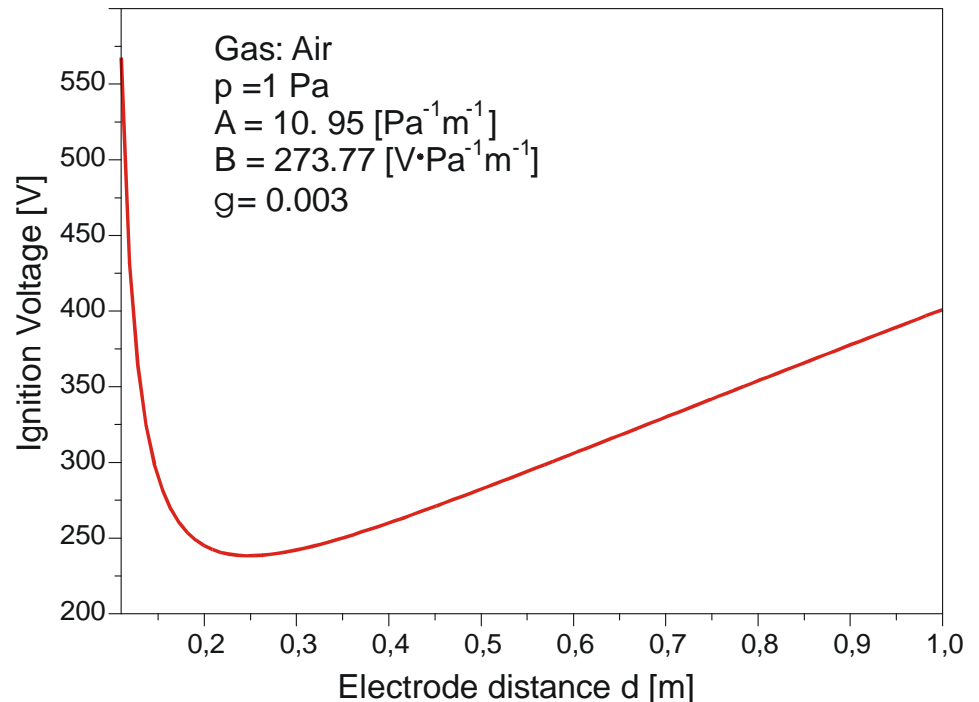
$$U = \frac{d \cdot W_{\text{el}}}{e \cdot \lambda} = 2 \text{ kV}$$

Paschen - Law

The relation between the **minimal electrode distance d**, the **ignition voltage U** and the **gas pressure p** to **ignite a gas discharge** is given by the **Paschen-law**:

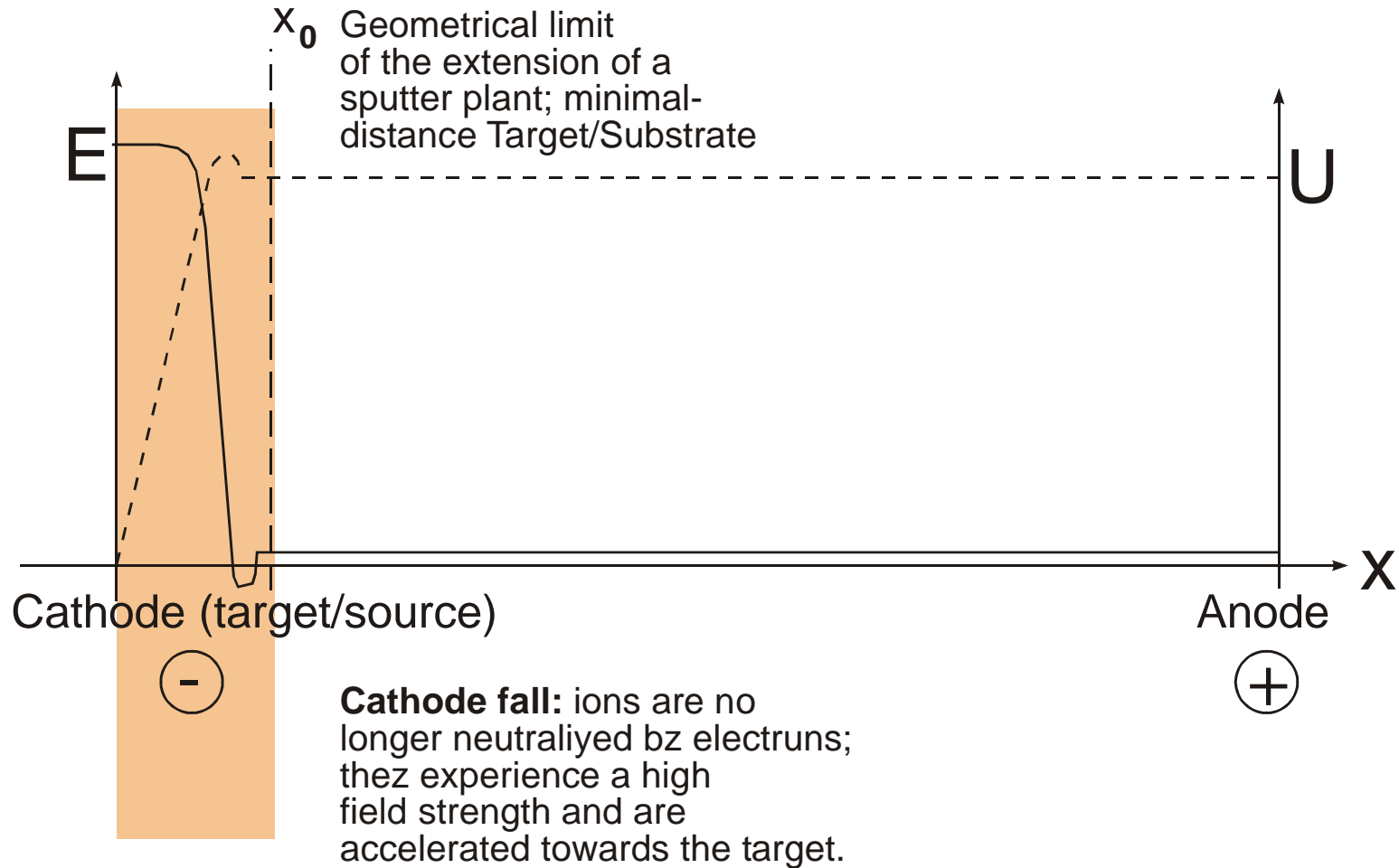
$$U = \frac{B \cdot p \cdot d}{\ln \left[\frac{A \cdot p \cdot d}{\ln(1/\gamma)} \right]}$$

A, B: empirical constants,
depending on the gas
 γ : Secondary electron
emission coefficient



Gas Discharge – Dark Space

Field and potential within the gas column:



Modifications of the Diode Discharge

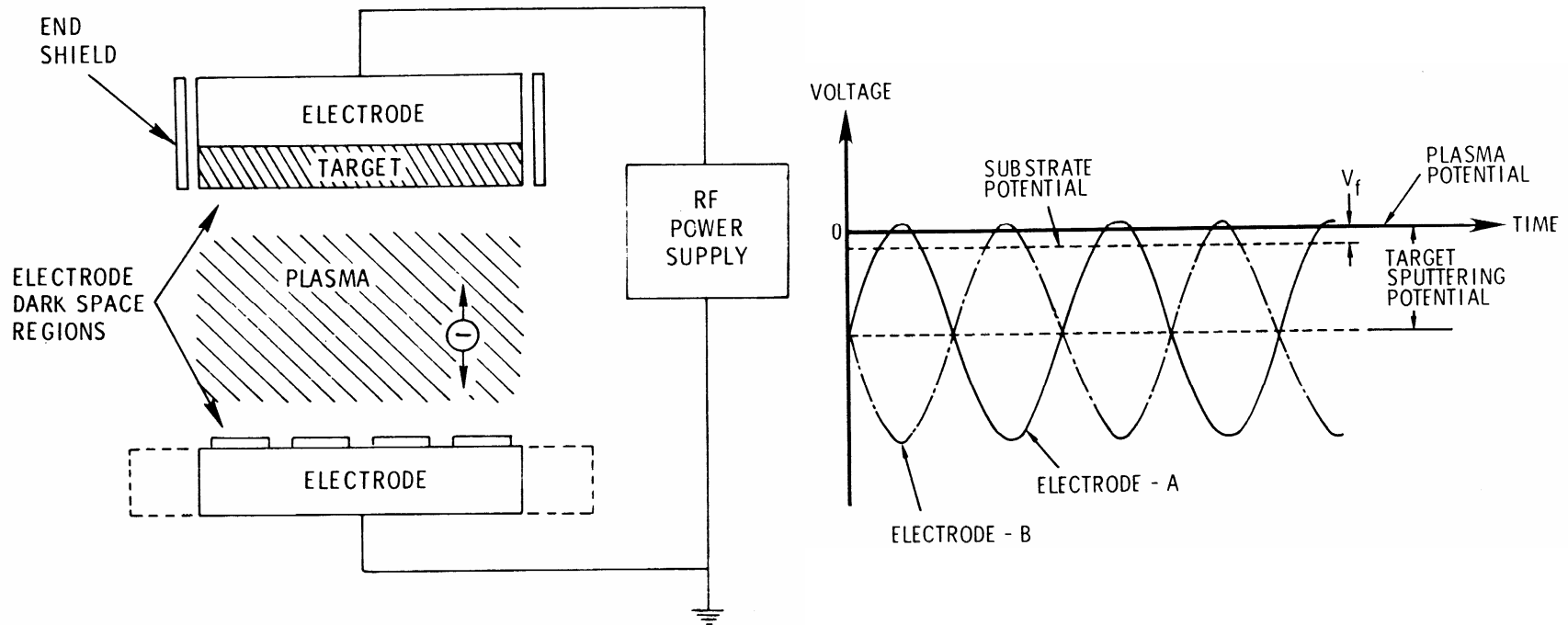
Aims:

- a) Minimize the extension of the dark space
- b) Increase of the ion current to maximize erosion rate
- c) Decrease of the working gas pressure (purity)
- d) Extension of the material class (semiconductor/insulator)

Modifications:

- RF-sputtering: c/d
- Triode sputtering: a-c
- Magnetron sputtering: a-c
- RF-magnetron: a-d
- Ionen beam sputtering: c; possibility to choose ion energy and direction

Radio Frequency Sputtering (RF-Sputtering) I



$f = 13,56$ MHz (open industry frequency)

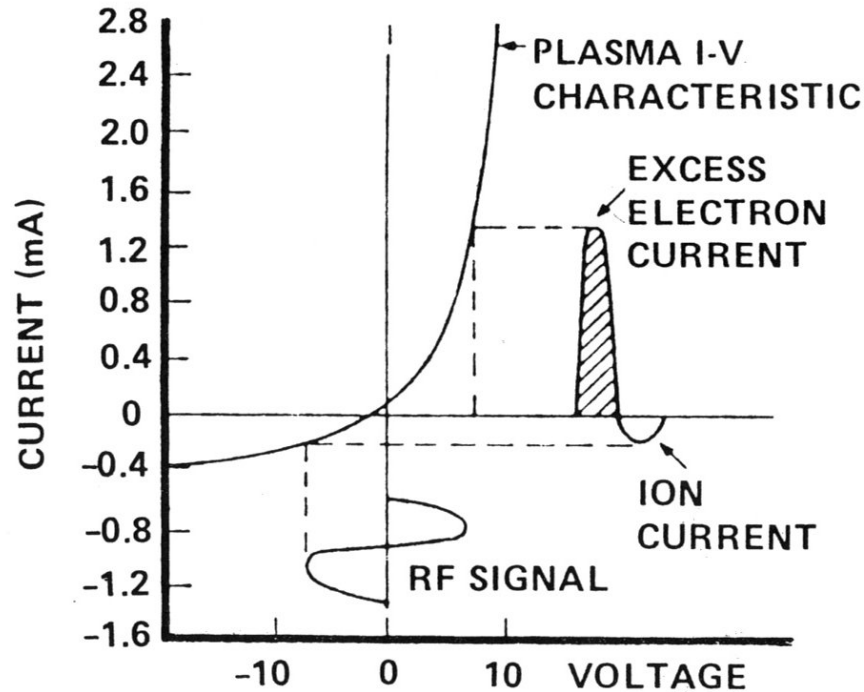
*** Higher electron density**

*** Insulators can be sputtered**

*** Gas pressure can be reduced**

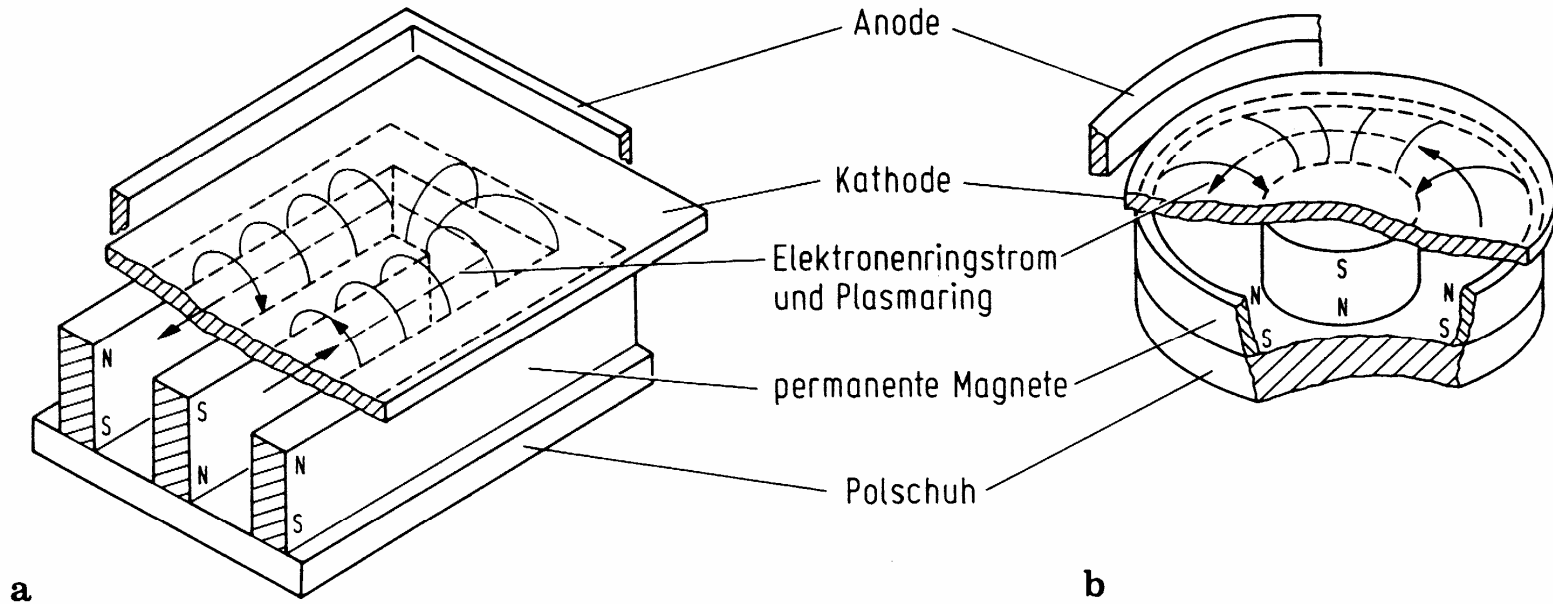
*** Different plasma characteristics (EEDF, Plasma potential)**

Radio Frequency Sputtering (RF-Sputtering) II



An excess electron current is generated by the higher electron mobility. It leads to a negative net voltage at the target, independent whether the target is conductive or not.

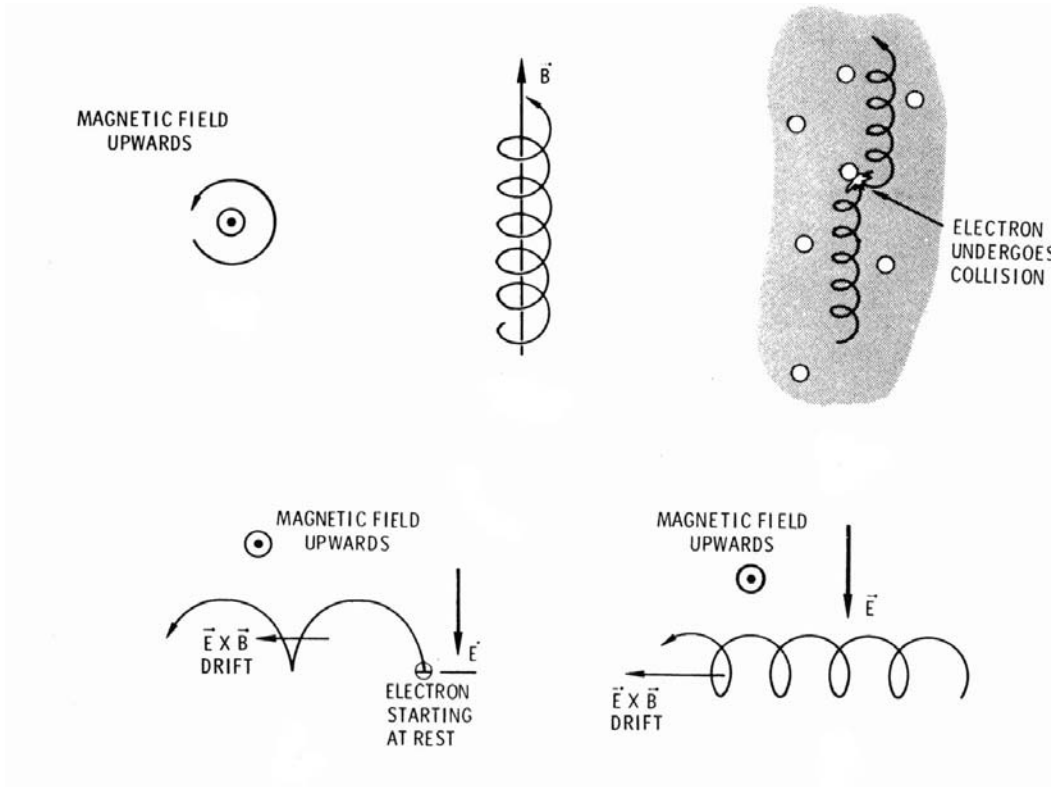
Magnetron-Sputtering, Basics I



Permanent magnets behind the target concentrate the plasma in the vicinity of the target.

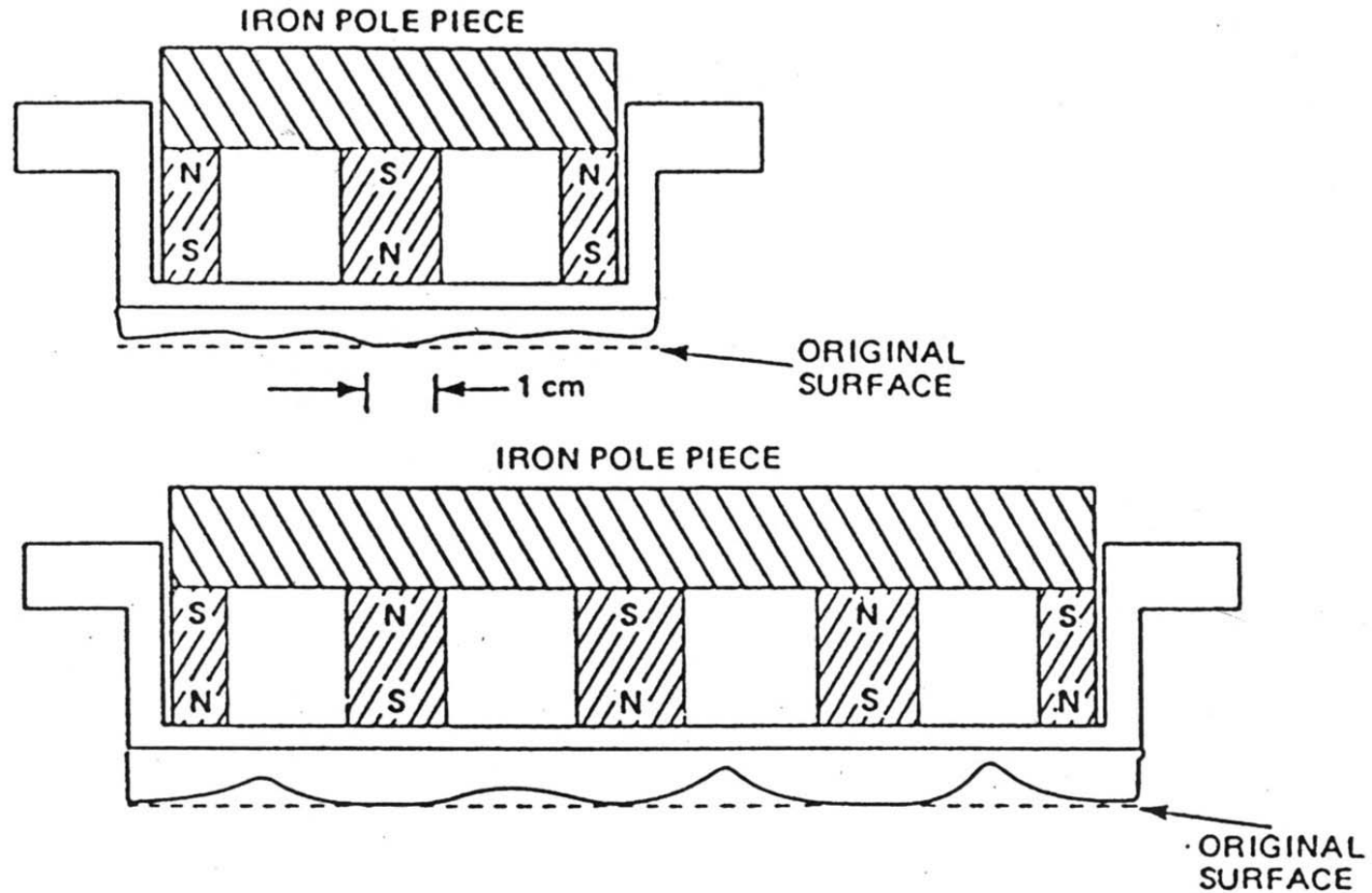
- * Extension of dark space is reduced**
- * Ion density is increased**
- * Gas pressure can be reduced**

Magnetron-Sputtering, Basics II

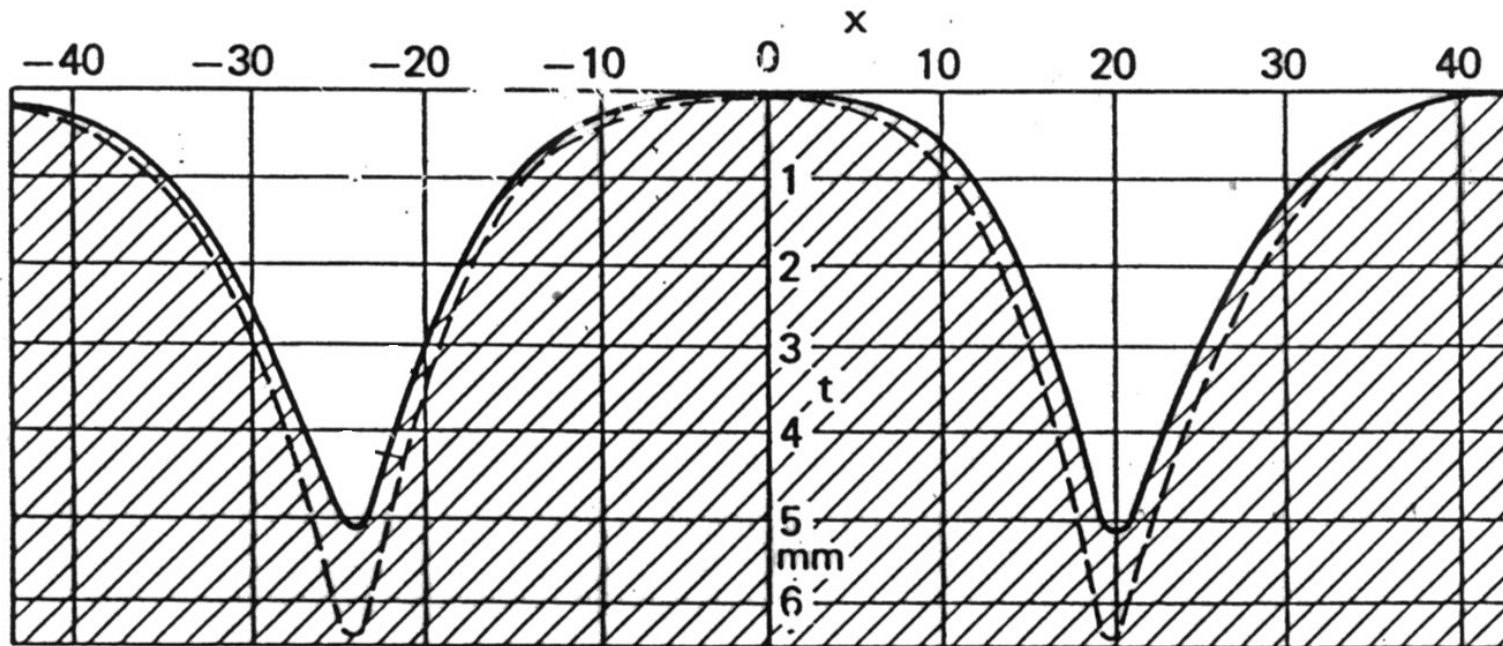


The magnetic field keeps the light electrons on spiral tracks (Lorentz-force) in the vicinity of the cathode. Therefore an electron can trigger a higher number of ionization events near the target.

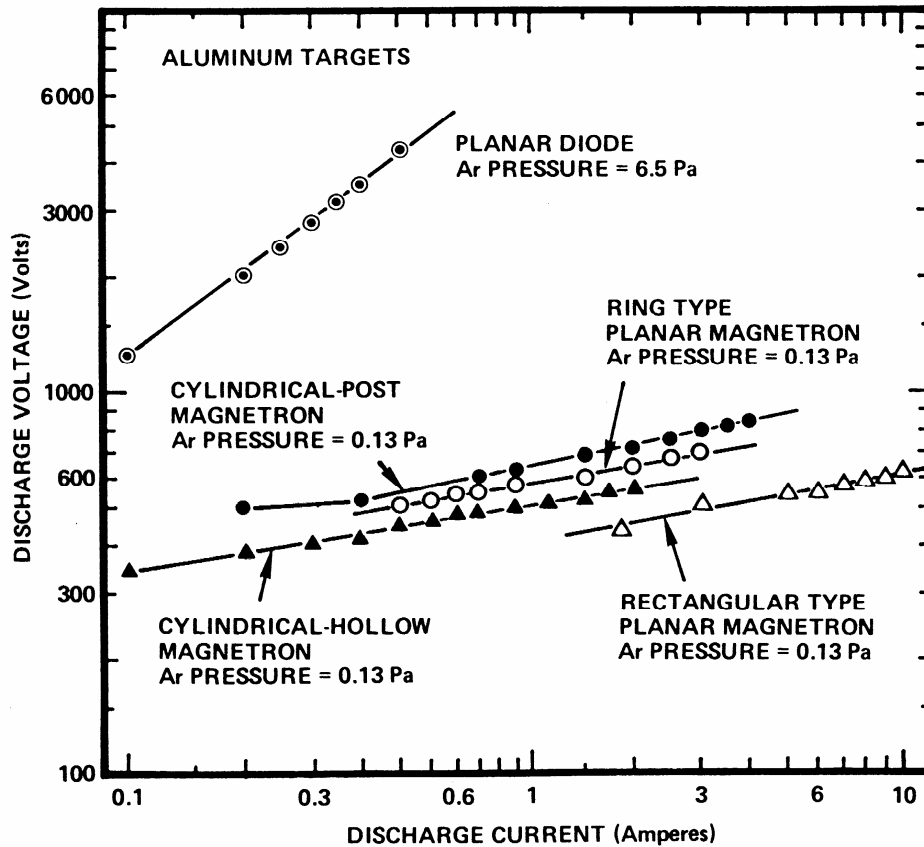
Magnetron-Sputtering: Magnetic Systems



Magnetron-Sputtering: Target Erosion



Magnetron-Sputtering: I/V Characteristics



Empirical correlation:

$$R \propto I(k \cdot \ln U)$$

R = Erosion rate

I = Discharge current

U = Discharge voltage

Magnetron discharges work at significantly lower gas pressures!